RESEARCH ARTICLE



Polyimide Aerogel Fibers with Controllable Porous Microstructure for Super-Thermal Insulation Under Extreme Environments

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Abstract

Application of aerogel fibers in thermal insulating garments have sparked a substantial interest. However, achieving a high porosity and low thermal conductivity for aerogel fibers remain challenging, despite the innovative designs of porous structure. Herein, we fabricated lightweight and super-thermal insulating polyimide (PI) aerogel fibers via freeze-spinning by using polyvinyl alcohol (PVA) as a pore regulator. The high affinity of PVA with water enables it to accelerate the ice crystal nucleation, adjust pore formation, and construct a controllable porous structure of PI aerogel fiber. The as-fabricated PI aerogel fiber has a considerable reduced pore size, high porosity (95.6%), improved flexibility and mechanical strength, and can be woven into fabrics. The PI aerogel fabric exhibits low thermal conductivity and excellent thermal insulation in a wide range of temperature (from -196 to 300 °C). Furthermore, the PI aerogel fabrics can be easily functionalized to expand their applications, such as in intelligent temperature regulation and photothermal conversion. These results demonstrate that the aerogel fibers/fabric are promising materials for next-generation textile materials for personal thermal management.

Keywords Polyimide · Aerogel fiber · Pore regulation · Thermal insulation · Thermal management

Introduction

Due to increasing demands of saving energy and a wide range of personal thermoregulation requirements, thermoregulating textiles capable of offering thermal management technologies are preeminently important nowadays [1-3]. Particularly, personal thermal-insulating textiles that could keep the human body thermally comfortable are essential in extreme environments such as Polar Regions and

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outer space [4–6]. However, traditional thermal insulation garments are mainly composed of cotton, down, and other filling materials, which are cumbersome and have poor thermal insulating effects [7, 8]. Therefore, developing novel, lightweight, and efficient personal thermal-insulating textiles is needed.

Low apparent density, ultrahigh porosity, and large surface area enable aerogels to block thermal conduction, convection, and radiation, making them an ideal thermalinsulating material [9–11]. Shaping the three-dimensional aerogels into one-dimensional aerogel fibers could apprehend the design and manufacturing of aerogel fabrics. Therefore, aerogel fibers and fabrics are expected to become the next generation lightweight, highly efficient thermalinsulating wearable garments. Recently, researchers have been working on aerogel fibers like inorganic silica aerogel fiber [12, 13] and organic aerogel fibers, such as Kevlar [14], silk [4, 15, 16], and cellulose aerogel fibers [17]. For example, Du et al. [12] prepared transparent silica aerogel fibers by reaction spinning, exhibiting a high specific surface area (890 m² g⁻¹), good thermal insulation, and broad temperature feasibility (- 196 to 300 °C), but their applications in wearable garments are largely limited due to low tensile strength (~150 kPa). Contrarily, the burgeoning

organic aerogel fibers have higher tensile strength compared to inorganic silica aerogel fibers. For instance, Kevlar aerogel fibers were fabricated through wet spinning from Kevlar nanofibrous dispersion, which presented excellent thermal insulation ability, high tensile strength (3.3 MPa), and high specific surface area [14]. Nevertheless, wet spinning often requires the troublesome solvent exchange and time-consuming supercritical drying to obtain the final aerogel fibers [18]. To overcome this, Cui et al. [4] reported a freeze-spinning method to fabricate silk aerogel fibers with an axially aligned porous structure, exhibiting excellent thermal insulation property. This freeze-spinning method combines "directional freezing" with "solution spinning", enabling large-scale and continuous fabrication of aerogel fibers with tunable porous structure, which makes it a potential strategy for preparing aerogel fibers and fabrics.

Polyimide (PI) fibers have attracted widespread attention due to their excellent tensile strength, high-temperature stability, and low-temperature flexibility [19, 20]. In our previous work, we used the freeze-spinning technique to prepare polyimide aerogel fibers having high tensile strength, excellent fire-retardanting ability, and good thermal-insulating performance [21]. However, the fabrics that are woven with the above-mentioned aerogel fibers still have higher thermal conductivity compared with inorganic silica aerogels. Therefore, the reduction of the thermal conductivity of the polyimide aerogel fibers/fabrics is crucial for their wider applications. Previous reports revealed that thermal transfer is closely related to the density, porosity, and pore size of the material [22]. Particularly, the pore size of aerogel fiber is a key factor affecting its thermal insulation behavior. Aerogels with smaller pore sizes can increase the number of solid-air interfaces, which resuls in multiple scattering at the interface and increases the path of solid thermal conduction that improves thermal insulation [23, 24]. Therefore, controllable construction of the pore size of aerogel fibers implicates the improved thermal insulating performance. Previous reports have shown that combining nanoparticles with a polymer solution or changing the freezing temperature could regulate the pore size of aerogels [25-28]. However, these methods require sophisticated equipment, and the agglomeration of nanoparticles hinders their applicability. Therefore, it is crucial to develop alternative strategies to regulate the pore size of aerogel fibers and improve relevant thermal insulation properties.

In this study, polyvinyl alcohol (PVA) was used as a pore regulator, to fabricate lightweight and super-thermal insulating PI aerogel fibers with controllable porous microstructure through freeze-spinning. PVA as an ice crystal nucleating agent can affect ice crystal growth and adjust pore size because of the abundant hydroxyl groups that exhibit high affinity with water molecules. The thermal conductivity of PI aerogel fabrics is optimized by adjusting the porous structure via PVA, achieving a low thermal conductivity of $28.7 \pm 2.0 \text{ mW m}^{-1} \text{ K}^{-1}$. Moreover, the PI aerogel fabric is flexible in an ultra-low temperature environment (– 196 °C) and can work under high temperatures (up to 300 °C). In addition, the PI aerogel fabrics could also function as intelligent temperature regulation and photothermal conversion fabrics when being incorporated with polyethylene glycol (PEG) and carbon nanotubes (CNTs), respectively. Therefore, the as-prepared PI aerogel fabric is potent as a lightweight personal thermal management garment in an extreme environment.

Experimental Section

Materials

Biphenyl 3,3',4,4',-teracarboxylic dyanhydride (BPDA, 99.0%), 4,4',-diaminodiphenyl ether (ODA, 98.0%), *N*,*N*-dimethylacetamide (DMAc, 99.0%), and triethylamine (TEA, > 99.5%) were all provided by Sinopharm Chemical Reagent Co, Ltd. Polyvinyl alcohol (PVA, $M_w \approx 80,000-124,000$) was acquired from Aladdin Chemistry Co., Ltd, China. Poly (ethylene glycol) (PEG, $M_w = 1000$) was supplied by Sinopharm Chemical Reagent Co. Multiwalled carbon nanotubes (CNT, length: > 10 µm) were purchased from Chengdu Organic Chemicals Co. Ltd.

Preparation of Polyimide (PI-x) Aerogel Fiber

According to our previous work, water-soluble poly(amic acid) (PAA) salt was synthesized from BPDA and ODA [29]. The PAA/PVA spinning solution was prepared by mixing PAA and PVA in aqueous solution. The weight ratio of PAA to water was fixed to 5:100, and the weight ratio of PAA to PVA was set to 10:1, 10:2 and 10:3. The PAA/PVA solution was magnetically stirred for 24 h to become a transparent and viscous PAA/PVA spinning solution. The PI aerogel fibers were prepared by freezespinning, freeze-drying, and subsequent thermal imidization. The PAA/PVA spinning solution was squeezed out through a pump-controlled syringe, through a temperature-controlled copper ring to freeze the gel fibers gradually, and finally collected by a collecting rod. At the end, the collected fibers were freeze-dried, and then thermally imidized in a tube furnace at 350 °C under an inert atmosphere to obtain PI aerogel fibers. The samples prepared with different mass ratios of PAA to PVA (10:1, 10:2 and 10:3) were designated as PI-10, PI-20 and PI-30, respectively.

Preparation of Composite Fabrics with Phase-Change Material (PCM)

The PI-20 aerogel fabrics were soaked in the PEG1000 and placed in vacuum oven with 70 °C for 12 h, for PEG1000 infusion into the PI aerogel fibers. Afterwards, the excess PEG1000 was removed by filter papers to obtain the final PI/PCM composite fabrics.

Preparation of Composite Fabrics for Photothermal Conversion

The PI-20 aerogel fibers were woven into a fabric (5 cm \times 5 cm), and CNT in isopropanol suspension (2 mg mL⁻¹) was sprayed on top of the PI-20 aerogel fabric surface repeatedly to ensure complete coverage and then dried under vacuum to obtain the PI/CNT composite fabrics.

Characterization

The microstructure of the PI aerogel fiber was investigated by field-emission scanning electron microscopy (FESEM, JSM-7500F, JEOL, Japan) operating at 5 kV. Mechanical properties of PI aerogel fibers/fabrics were tested by an electronic universal testing machine (UTM2102, Suns Technology Stock Co., Ltd, China) with a sensor of 50 N. All thermal images were acquired via a thermal imager (TiS40, Fluke Co., Ltd, USA) at working distance of 20 cm. The thermal conductivity (λ) of PI aerogel fabrics at different temperatures was measured with a hot disk thermal analyzer (Hot Disk TPS 2500S, Sweden). The thermogravimetric analysis (TGA) was performed by a thermogravimetric analyzer (F1 Libra, Netzsch Co., Ltd, German) with heating rate of 10 °C min⁻¹. The phase change enthalpy was computed on a differential scanning calorimeter (DSC-822, Sweden) with heating rate of 10 °C min⁻¹. The temperature-time curves were recorded by the thermal couple (175T2, testo Co., Ltd, China). The porosities of PI aerogel fiber were calculated using the following equation:

$$P = \left(1 - \frac{\rho_0}{\rho}\right) \times 100,$$

where P is the porosity, ρ_0 is the apparent density, and ρ is the skeletal density, which is estimated from the density of polyimide (1.4 g cm⁻³).

Results and Discussions

The fabrication process of PI aerogel fibers and fabrics is schematically illustrated in Fig. 1a, which involves freeze-spinning, freeze-drying, thermal imidization and weaving. The PAA/PVA spinning solution was first extruded through a syringe, before being passed through a temperature-controlled copper ring to gradually freeze the gel fibers. The frozen fibers were gathered on a collecting rod and then freeze-dried to remove ice crystals to achieve its porous structure. PAA was transformed into PI during the subsequent thermal imidization at 350 °C, while the PVA was removed because its decomposition began at ~ 280 °C (as shown by TGA curve in Fig. S1a), leaving the pure PI aerogel fiber [30–32]. Furthermore, FTIR spectra reveal the characteristic peaks at 3293 cm⁻¹ (-OH stretching vibration) and 2911 cm⁻¹ (-CH₂ asymmetric stretching vibration) for pure PVA (Fig. S1b) [33]. However, the characteristic peak of PVA in the FTIR of PI-20 disappeared, which also proved that PVA was completely removed after thermal imidization. The light weight PI aerogel fibers are highly porous (95.6% porosity) and have low density (0.06 g cm^{-3}) . Figure 1b depicts the image of the as-prepared PI aerogel fibers in a roll with approximately 400 µm diameter and yellow color. Photograph of PI aerogel fiber knot displays the good flexibility and knittability of aerogel fibers (Fig. 1c). Moreover, the fiber shows high tensile strength and can withstand 200 g tensile load (Fig. 1d). Due to the outstanding flexibility and mechanical strength, the fiber could conveniently be woven into fabrics, providing the possibility for practical use in garments (Fig. 1e and Fig. S2).

The formation and growth of ice crystals in freezespinning process determines the micro-morphology of the aerogel fiber, similar to the ice template method [34]. The cross-sectional microstructure of PI aerogel fibers with different content of PVA in the spinning solution is revealed by SEM images in Fig. 2a-h. All the aerogel fibers exhibit a three-dimensional porous structure and different pore sizes that vary by changing the amount of PVA. The pure PI-0 aerogel fiber has large pore sizes $(46.3 \pm 12.6 \mu m)$ with broad distribution (Fig. 2a, b and Fig. S3a). With the incorporation of PVA, the pore size of PI-10 aerogel fibers decreases to $41.5 \pm 20 \,\mu\text{m}$ (Fig. 2c, d and Fig. S3b). The PI-20 aerogel fiber with initial 20 wt% PVA exhibits the smallest pore size centered in $11.5 \pm 4.5 \ \mu m$ among those samples (Fig. 2e, f and Fig. S3c). However, further increase in the amount of PVA leads to the curved laminar porous structure as for PI-30 aerogel fiber, which is probably due to the fact that excess PVA promotes the nucleation and formation of ice crystals, forming lamellar ice crystals [35] (Fig. 2g, h and Fig. S3d). The surface of



Fig.1 Fabrication of PI aerogel fibers and fabrics. **a** Schematic description of the fabrication process of PI aerogel fibers and fabrics. **b** Photograph of the PI aerogel fiber collected in a roll. **c** Pho-

tograph of PI aerogel fiber knot. **d** Photograph of a single PI aerogel fiber withstand weight of 200 g. **e** Photograph of a PI aerogel fabric $(10 \text{ cm} \times 10 \text{ cm})$, reflecting its folding property

aerogel fibers is also uniformly porous structure, with the pore size decreasing as the PVA concentration increases (Fig. S4). The smaller pore size of PI-20 aerogel fibers is attributed to the strong interaction between PAA and PVA as well as PVA and water, as schematically illustrated in Fig. 2i. The interaction between the PAA chain and PVA can be deduced from the FTIR characterization (Fig. 2j). The strength of the hydroxyl absorption peak (3100–3650 cm¹) increases in PAA/PVA compared to PAA, whereas the wavenumber of the CO-NH bond decreases, showing a substantial interaction between PVA and water as well as PAA and PVA [36]. To further demonstrate the interaction between PAA and PVA, the rheological behaviors of the PAA and PAA/PVA solutions were carried out using a rotational rheometer as shown in Fig. S5. The viscosity of PAA/PVA increased significantly with increasing PVA content, demonstrating a strong interaction between PAA and PVA [37]. Due to the high affinity between PVA and water, it could accelerate the ice nucleation and increase the amount of ice crystals, resulting in smaller ice crystals and thus smaller pore size [35, 38]. This smaller pore size could significantly improve the thermal insulation of aerogel fibers.

The PI aerogel fibers, with up to 95.6% porosity, have a tremendous potential in the field of thermal insulating garments. PI aerogel fibers with diverse porous structures were placed on the same hot stage to compare their thermal insulating properties. Infrared images were captured at various temperatures ranging from - 30 to 300 °C, with three representative infrared images displayed in Fig. 3a, showing its advantages over a wide temperature range. The temperature difference $(|\Delta T|)$ between the PI aerogel fiber surface and the thermal platform is estimated and summarized in Fig. 3b via infrared images. With the decrease of pore size, the $|\Delta T|$ increases, which indicates that smaller pores promote thermal insulation (Fig. 3c). However, the PI-30 aerogel fibers have higher $|\Delta T|$ because the curved laminar porous structure can reduce the thermal conduction, at the same time it can form multiple thermal reflection interfaces. Figure 3d schematically illustrates the heat transfer through the aerogel fiber. Typically, thermal conductivity of aerogel fiber (λ_{fiber}) is the sum of the thermal convection ($\lambda_{conv.}$), thermal conduction ($\lambda_{cond.}$), and thermal radiation $(\lambda_{rad.})$ [4]. The thermal convection $(\lambda_{conv.})$ of aerogel fiber is extremely limited because airflow is suppressed in microsized pores. The thermal radiation ($\lambda_{rad.}$) is negligible owing



Fig. 2 Morphological and chemical structural characterization of PI aerogel fibers. **a**–**h** SEM images of PI aerogel fibers with different initial content of PVA. **a**, **b** PI-0; **c**, **d** PI-10; **e**, **f** PI-20 and **g**, **h** PI-30. **i**

Schematic illustration for porous structure of aerogel fiber and interaction between PAA and PVA chains. **j** FTIR spectra of the PAA/ PVA aerogel fibers with different contents of PVA

to the relatively low environment temperature [39]. The heat exchange via thermal conduction $(\lambda_{cond.})$ is determined by solid conduction (λ_s) and gas conduction (λ_{α}), and strongly depends on the pore size. Reduction in the pore size can extend the path of solid conduction and reduce the movement of gas molecules. Furthermore, smaller pore size contributes to numerous solid-air interfaces that lead to multiple scattering at interfaces, resulting in reduced thermal conduction ($\lambda_{cond.}$) of aerogel fibers. Therefore, pore size reduction can enhance the thermal insulation performance of the aerogel fiber. Moreover, mechanical properties are crucial for knittability and wearability of the aerogel fibers. Typical stress-strain curves for single PI aerogel fibers are shown in Fig. 3e. As the pore size decreases from $46.3 \pm 12.6 \,\mu\text{m}$ to $11.5 \pm 4.5 \,\mu\text{m}$, the tensile strength raises from 2.1 ± 0.5 to 5.2 ± 0.3 MPa. At the same time, the modulus of PI-20 aerogel fiber is increased to 35.2 ± 4.0 MPa (Fig. 3f). These results demonstrate that reducing the pore size dramatically augments the thermal insulation and mechanical properties of aerogel fibers.

We further demonstrated the mechanical and thermal insulating performances of the PI aerogel fabric woven by PI-20 aerogel fibers. The PI aerogel fabric (weight 400 mg, size $100 \text{ mm} \times 15 \text{ mm} \times 2 \text{ mm}$) could bear a load of more than 1250 times its own weight without damage, as presented in Fig. 4a. Typical stress-strain curves for PI aerogel fabrics demonstrate a tensile strength of 2.2 ± 0.2 MPa, as shown in Fig. S6. Furthermore, the PI aerogel fabric can be folded and released repeatedly in liquid nitrogen without any damage (Fig. 4b) and Video S1, illustrating its outstanding flexibility in the low temperature environment. For thermal insulation applications, the PI aerogel fabric is placed on a thermal platform and compared to commercial cotton and polyester fabric (Fig. 4c). At a stage temperature of 300 °C, the PI aerogel fabric was thermally stable with decomposition temperature of up to 500 °C (TGA curves shown in Fig.



Fig. 3 Mechanical and thermal insulating property of PI aerogel fibers. **a** Infrared images of PI aerogel fibers with different porous structures on thermal platform with different temperatures. **b** Temperature difference ($|\Delta T|$) between the PI aerogel fiber surface and the thermal platform, at various platform temperatures ranging from – 30 to

300 °C. **c** Temperature difference ($|\Delta T|$) is correlated with the pore size of corresponding PI aerogel fibers. **d** Schematic diagram of heat transfer of the aerogel fiber. **e** Tensile stress versus strain curves and **f** modulus of PI aerogel fibers

S7) and its average surface temperature was 220 °C. Contrarily, the cotton pyrolyzed and polyester melted on the stage after 3 min, as can be inferred form the corresponding TGA and DSC curves (Fig. S8). As obvious by the temperature difference ($|\Delta T|$) in Fig. 4d, The PI aerogel fabric showed a higher $|\Delta T|$ than cotton and polyester form – 30 to 300 °C, indicating its excellent thermal insulation performance over a wide temperature range (Fig. 4d). The corresponding thermal conductivity of the PI aerogel fabric was only 28.7 ± 2.0 mW m⁻¹ K⁻¹ at 25 °C and slightly increased as the temperature raised to 300 °C (Fig. 4e). Besides, the thermal insulating property of the PI aerogel fabric exhibited longtime stability under high and low temperature environment, without temperament fluctuation (Fig. S9). As an example, a hand could be placed on ice or a hot stage with 100 °C with a piece of PI aerogel fabric (Fig. S10), demonstrating its great potential as thermal protective clothing.

On the same wrists, PI aerogel fabric (thickness: 4 mm) is compared with cotton fabric (thickness: 4 mm) to further demonstrate the wearability and thermal insulation of aerogel fabrics. The infrared thermal imager did not detect the wrist covered by PI aerogel fabric, proving its infrared thermal stealth function, which is expected to be applied to the infrared thermal stealth garments for soldiers [40]. The temperature difference ($|\Delta T|$) between the surface of PI aerogel fabric and the skin is as high as 10.8 °C that is twice that of cotton fabric, indicating the excellent thermal insulating properties as clothing for practical use (Fig. 4g).

In addition to preventing the heat transfer, the PI aerogel fabrics must be breathable in order to improve human comfort (Fig. S11a). We compared the breathability of PI aerogel fabrics with commercial cotton fabrics. Hot steam can pass through the PI aerogel fabrics smoothly and the amount of water vapor in the upper part of the beaker is almost equivalent to that of cotton (Fig. S11b). As for the water vapor transmission rate, the air permeability of the PI aerogel fabrics is comparable to that of cotton fabrics (Fig. S11c). At the same time, the hydrophobicity of the PI aerogel fabrics (water contact angle of 101.7°) further improves the wearing comfort (Fig. S11d). Therefore, the PI aerogel fabrics are hydrophobic and breathable, which can meet the requirements for human wearing.

The PI aerogel fabrics can be easily functionalized to broaden the horizon of their applications, such as intelligent temperature regulating and photothermal conversion. The PI aerogel fabrics can be combined with PCM such as PEG for temperature regulation in the microclimate near the human skin, providing comfortable temperature environment for the human body [41]. Due to its high porosity and strong capillary force, the PI aerogel fiber can load high content of PEG



Fig. 4 Mechanical and thermal insulating performances of the PI aerogel fabric. **a** Photograph shows the PI aerogel fabric withstanding a tensile load of 500 g. **b** Photograph of the PI aerogel fabric immersed into liquid nitrogen with subsequent folding and release. **c** Photograph and infrared images of the PI aerogel, cotton and polyester fabrics placed on the 300 °C thermal platform for 3 min. **d** Tem-

perature difference ($|\Delta T|$) between the fabric surface and the thermal platform are correlated with different fabrics. **e** Thermal conductivity (λ) of the PI aerogel fabric at diverse environmental temperatures. **f** spectra images of PI aerogel fabric and cotton fabric covered on skin, and **g** corresponding surface temperature of bare skin, cotton and PI aerogel fabric

without leakage during use. The TGA curves display that the loading content of PEG is 91.3% (Fig. S12a). At the same time, the DSC curve of the PI/PCM composite fabric is shown in Fig. S12b, demonstrating the high energy storage performance with phase change enthalpy of 161.2 J g⁻¹. The temperature regulating ability of PI/PCM composite fabric was detected by simulating the change of external temperature with the hot stage, and the device is schematically illustrated in Fig. 5a. The surface temperature change of PI/PCM composite fabric was detected by infrared thermal camera in Fig. 5b. Upon heating for 5 min, the surface temperature of the PI/PCM

composite fabric was only 41.0 °C, while that of PI aerogel fabric rapidly increased to 48.0 °C. After cooling for 5 min, the surface temperature of the PI/PCM composite fabric remained 35.4 °C, while that of PI aerogel fabric rapidly decreased to 27.0 °C (Fig. S13). This is mainly due to the phase change of PEG, which can delay the temperature change during the external temperature variation [42]. However, the final surface temperature of PI/PCM composite fabric (55.6 °C at 15 min) is higher than that of PI aerogel fabric (52.6 °C at 15 min), due to the low thermal conductivity of PI aerogel fabric. To further suppress the heat loss, a double-layer fabric is proposed



Fig. 5 Multifunctionality of the composite fabric. **a** Schematic illustration of the device for testing the thermal regulation of the PI/PCM composite fabric. **b** Infrared images showing the PI/PCM composite fabric over heating–cooling cycle (25–80 °C). **c** Schematic illustration of the device for the double-layer fabric. **d** Infrared images showing the double-layer fabric over a heating–cooling cycle (25–80 °C).

e Temperature–time curves of the surface of composite fabrics with stage temperature changing. **f** Schematic diagram showing the photothermal conversion of the PI/CNT composite fabric. **g** Surface temperature changes of the PI/CNT composite fabric and PI aerogel fabric being exposed to 100 mW cm⁻² light irradiation for 15 min

by combing PI aerogel fabric and PI/PCM composite fabric to achieve the bifunctionality of temperature regulation and thermal insulation, as illustrated in Fig. 5c. The surface temperature change of double-layer fabric was detected by infrared thermal imager in Fig. 5d and plotted in Fig. 5e. The infrared images show that the upper surface temperature of the doublelayer fabric is lower than that of the one-layer PI/PCM fabric during the heating process, due to the thermal insulating ability of the PI aerogel fabric. During the cooling process, the temperature of double-layered fabric decreased slowly, which can be maintained at about 30 °C even if the external temperature is 20 °C. This double-layer fabric could effectively suppress heat loss and regulate heat during the external temperature changes, making it promising candidate for highly efficient personal thermal management clothes. In addition, composite fabric for photothermal conversion was prepared by spraying CNTs on the surface of PI aerogel fabric for human heating. The experimental device for photothermal conversion of the composite fabric was illustrated in Fig. 5f. The PI/CNT composite fabric and PI aerogel fabric were exposed to 100 mW cm⁻² light irradiation for 15 min and then the light was removed, and the temperature was detected by infrared thermal imager as plotted in Fig. 5g. As observed, the temperature rising speed of PI/CNT composite fabric is significantly higher than that of PI aerogel fabric under light irradiation, proving its good photothermal conversion ability that is attributed to the better light-absorbing ability of CNT [43, 44]. In addition, CNTs are evenly distributed and adhered firmly on the PI aerogel fabric, which can be washed in water (Fig. S14), making it practically applicable. Therefore, the PI aerogel based composite fabrics with multi-functionality are potential smart material for intelligent thermal management.

Conclusions

In conclusion, using freeze-spinning, PI-20 aerogel fibers with high porosity (95.6%), good mechanical, and thermal insulating properties have been fabricated from PAA/PVA solution. The pore size of PI aerogel fiber can be reduced

from 46.3 ± 12.6 to $11.5 \pm 4.5 \,\mu$ m using PVA as an ice crystal nucleating agent. The PI aerogel fabric woven from the PI aerogel fibers exhibits low thermal conductivity and excellent thermal insulation at extremely low temperature (- 196 °C), such as liquid nitrogen, and high temperature (300 °C); owing to its small pore size and high porosity. Furthermore, the PI aerogel fabrics can be easily functionalized with PCM or CNT, to prepare intelligent temperature regulating or photothermal conversion fabric, further expanding their potential applications in personal thermal management. In addition, our strategy of using PVA as a pore regulator is simple and efficient, providing alternative method for preparing porous materials.

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Declarations

Conflict of interest The authors declare no competing financial interest.

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